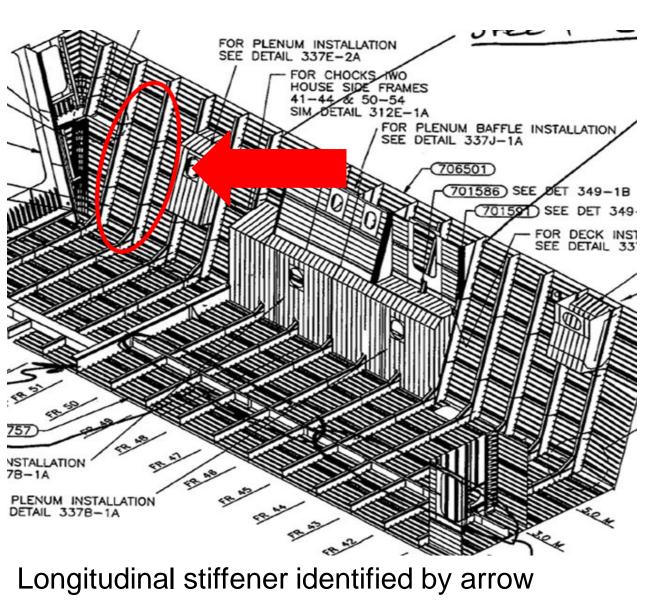


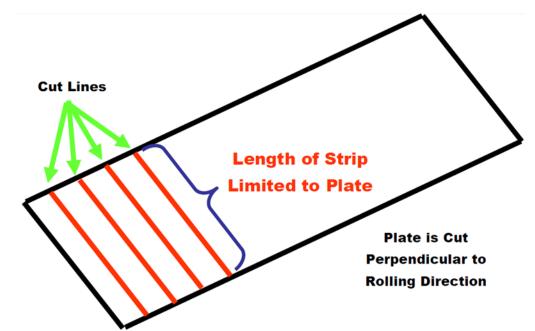
FLEXURAL BEHAVIOR AND ASSESSMENT OF ALUMINUM STIFFENERS USED ON UNITED STATES NAVY LITTORAL COMBAT SHIP (LCS).

Background

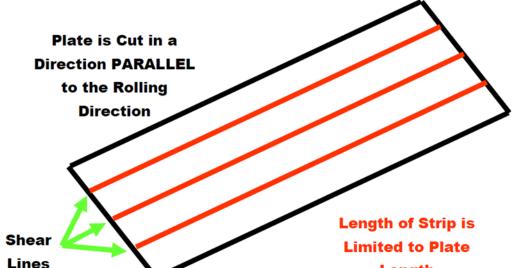


- Aluminum Alloy 5083 stiffeners are currently used on the LCS hulls and superstructure.
- The traditional method of production is to cold form the angle to 90 degree.
- Typically member length produced is limited to six feet
- Resulting in multiple splices to achieve a usable length and frequent distortion due to the imperfect nature of Gas Metal Arc Weld(GMAW)

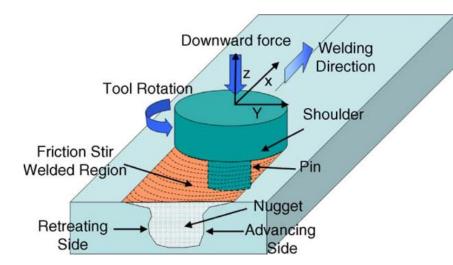
Introduction



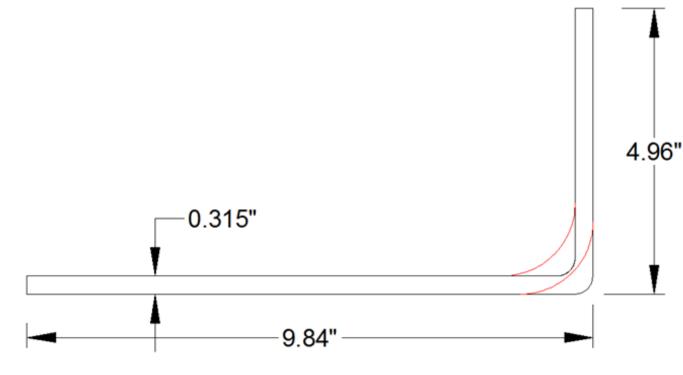
Model of perpendicular cut locations required for cold-forming (Smith, et al. 2009)



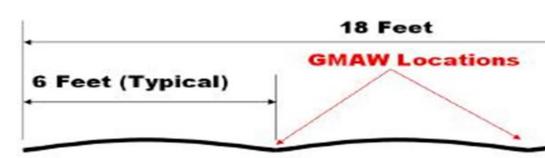
Model of parallel cut locations allowed for FSP (Smith, et al. 2009)



Schematic of FSW Process (Mishra and Ma 2005)



Cross-section of LCS stiffener



Traditional Method Production

- Cut Perpendicular to rolling action
- Multiple splicing
- HAZ cause warping

18 Feet

Future Method Production

- Cut Parallel to rolling action
- Angle Bent parallel to rolling action
- Longer stiffener members are produced
- Production Increases and Cost Falls



LCS Panel with Stiffener attached

Paul Betone: Oglala Lakota College Faculty Advisors Dr. Damon Fick Research Experience for Undergraduates – Summer 2013



Broader Impact

In the future the United States Navy expects to produce a total of 60 to 70 of the LCS platform ships. With the new method in using the FSP to create the longer members of the aluminum alloy 5083 stiffener, the pace of production will speed up and cost of building the ships could be reduced. Thus having a significant impact on future engineering of ship building.

Objective

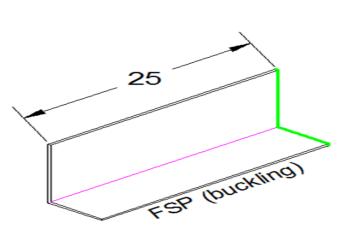
- Develop a four-point test for flexure and instrumentation strategy
- •Compare the response of the FSP angle to the traditional method of production
- •Evaluate the performance of a gas metal arc weld splice and a friction stir weld splice
- Identify any correlations with tests done previously involving tensile coupon test and compression buckling test.

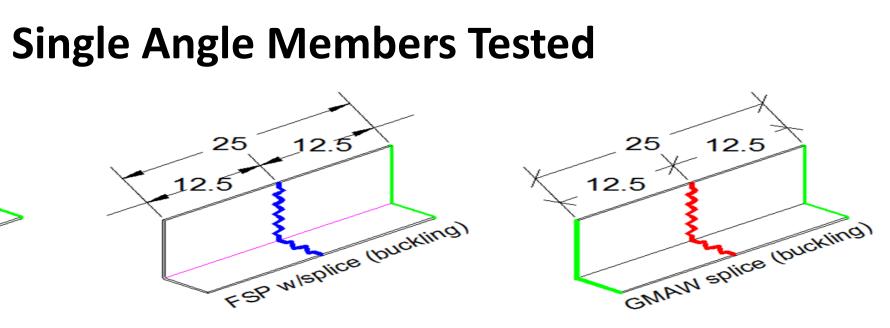
Special Thanks to Dr. Michael West, Dr. Damon Fick, and Dr. Alfred R. Boysen - National Science Foundation DMR-1157074

Procedures

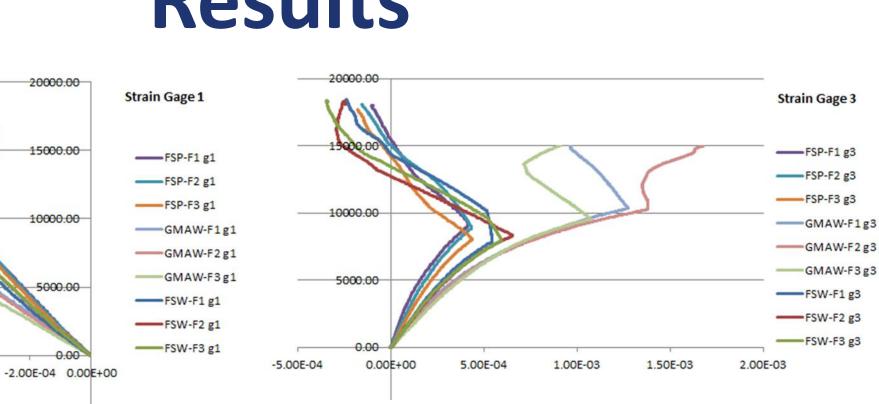
Instrumentation Design & Installation

- Tinus Olsen 300 kip load frame measurements. Data Acquisition/Programming using National Instruments Lab Signal Express Software
- Four-point flexure testing to evaluate specimen strains and displacement response.





Results



Specimen tested FSP-F1 FSP-F2 FSP-F3 GMAW-F1 GMAW-F2 GMAW-F3 FSW-F1 FSW-F2 FSW-F3

7.7 7.7 8.2 8.3 7.8 7.9

Strain Gage 3

9.0

8.8

7.9 10.2

10.2

9.5

Contact Load (KIPS)

Strain Gage 1

9.0

9.0

7.9

10.2

10.2

9.4





Contact Strain	
Strain Gage 1	Strain Gage 3
-3.88E -04	4.09E -04
-3.86E -04	4.27E -04
-3.57E -04	4.28E -04
-6.98E -04	1.26E -03
-6.98E -04	1.37E -03
-8.80E -04	1.06E -03
-4.18E -04	5.30E -04
-4.15E -04	6.46E -04
3.95E -04	5.87E -04

Conclusions

• Strain Gage 1 and 3 show the stiffness of the new fabrication method as the trends of the Strain vs Load Data indicates a steeper slope for the New Method of Production Short leg of GMAW specimens was approximately "27%" less stiff than the FSP and FSW specimens measured by the slope of the load-strain curves Long leg of GMAW specimens made contact with steel platen at approximately 2500 lbs higher than FSP and FSW specimens